

been calibrated under pressure and displacement measure-

tic pressure loading, was Since the pressure has only (~1% at 10 kbar), the As a result, it was possible within a few per cent as deter-

ably in the pressure vessel by small fuse wires. After ed, the load was applied by In this way the "constant" elongated to mechanical in a small fraction of a sus time on a Leeds and

ee-point loading constructed

ene film (0.002 in. thick). ally. The stress distribu- the viscoelastic analysis t much of a problem for a ylene does not fall in this nsile tests. Qualitatively, at of tests.

m. Samples were cut and

(1)

width, T is the sample thick- extension. The results of ures is shown in Figure 1. e mean stress is increased, observation applies to both ore, creep rates were gen-

ly different results. As rmined from sample geo-

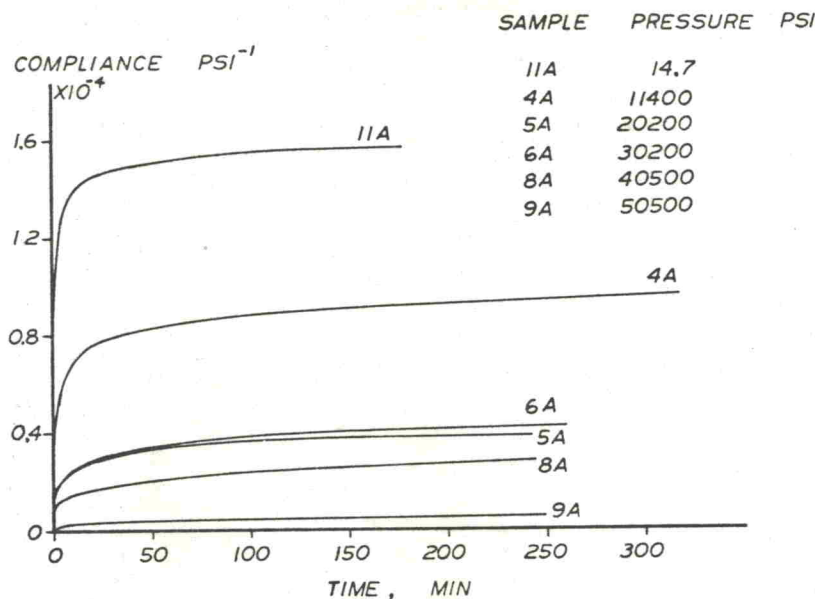


Fig. 1. Compliance of polyethylene as a function of hydrostatic pressure as determined from creep tests.

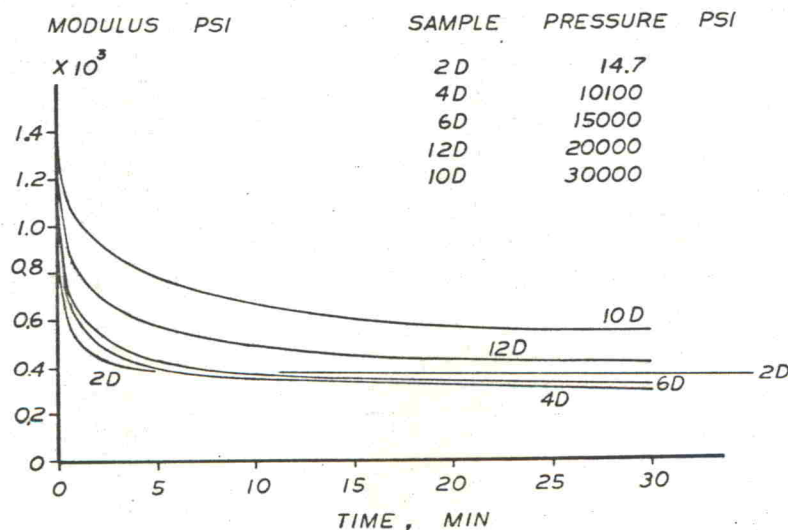


Fig. 2. Modulus of polyethylene vs. hydrostatic pressure as determined from stress relaxation tests.

metry and the measured sample force by the equation

$$E(t) = \frac{W(t)/dT}{\Delta l/l} \quad (2)$$